Commercial Kitchen Ventilation

Optimizing System Performance





What can make a hood work better?

9 times out of 10 it is <u>NOT</u> more exhaust!

What's wrong with this installation?



Could This Hood Be Improved?



... or this one?



... or this one?



... close that gap!



...and add that side panel!

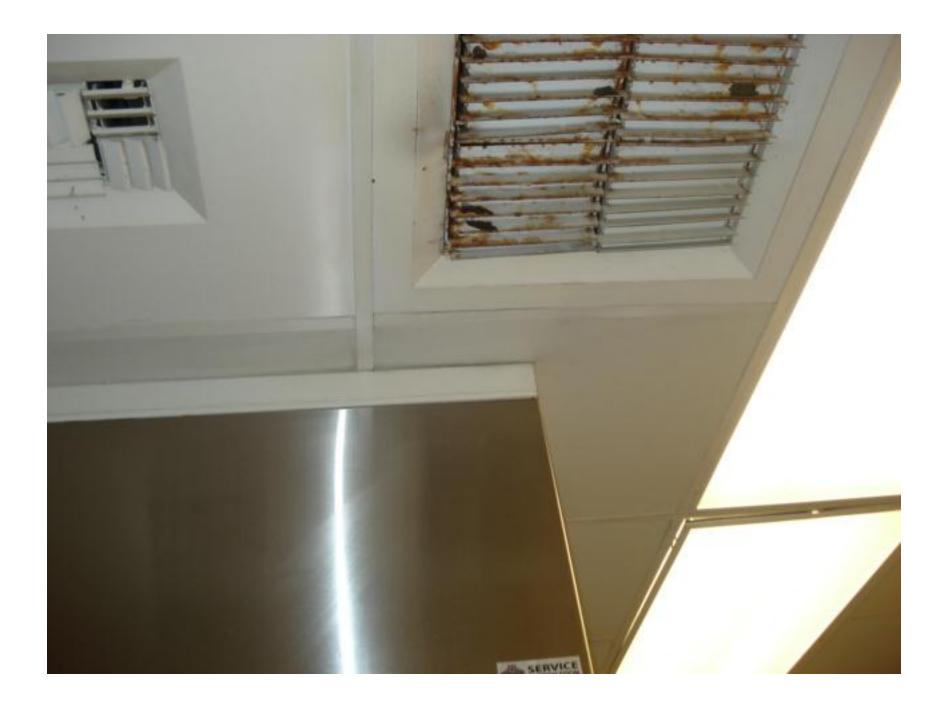




There are hoods everywhere that would benefit from a side panel











QSR tries a single canopy hood



Total exhaust = 2200 cfm

...but back to a 2-hood system



Total exhaust = 1600 cfm



LEED design for another QSR

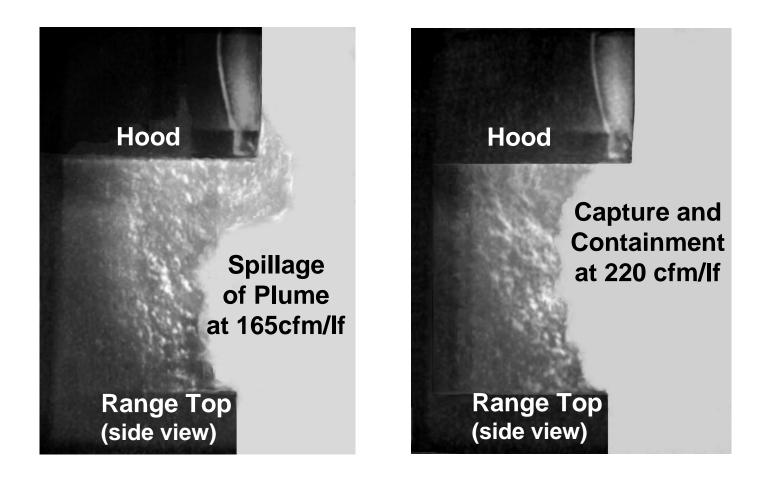
30% Design STRATOUEM Airflow Reduction with DVC (temp or



Exhaust Airflow = 600 - 1200 cfm

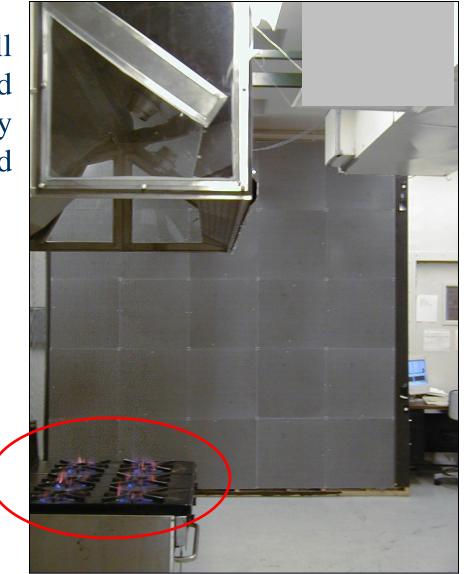
Food Service Technology Center has its own Commercial Kitchen Ventilation Lab

Schlieren Flow Visualization

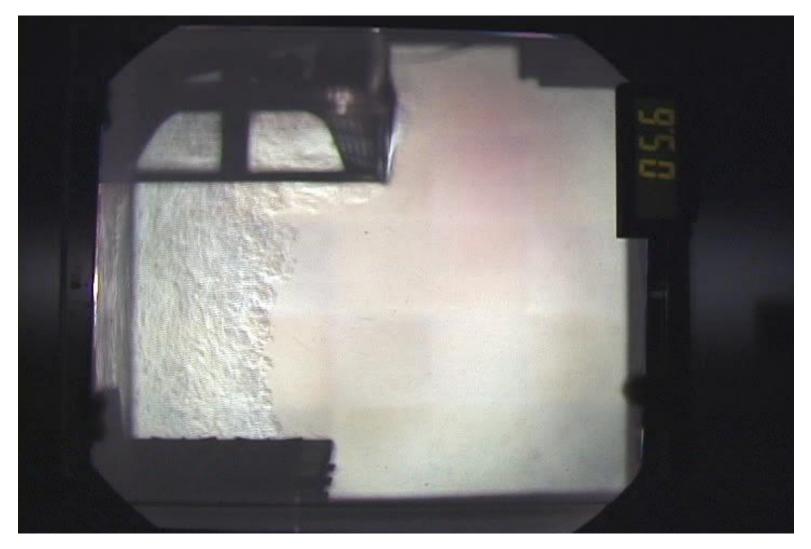


What the Eye Sees!

8-Ft Wall Mounted Canopy Hood

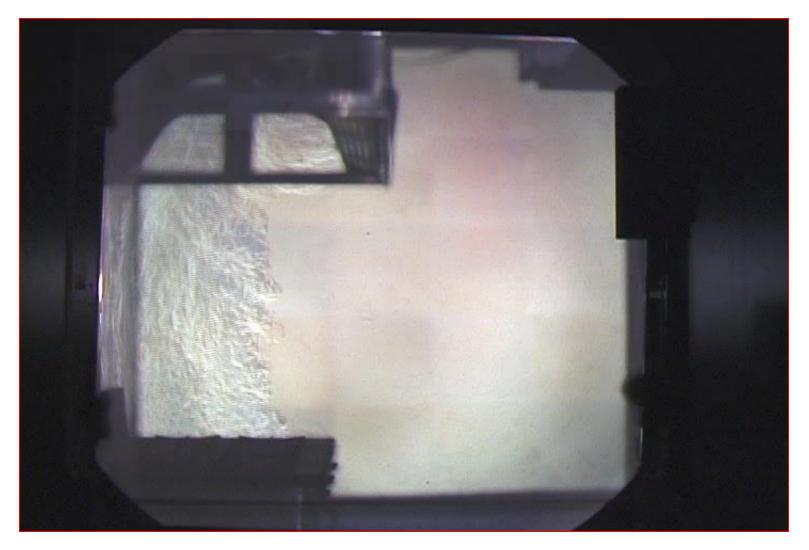


What the Camera Sees!



Hood Does Not Capture & Contain

Makeup Air Introduced at Low Velocity



Capture & Containment (C&C) @ 1400 CFM

CKV Optimization Strategies :

1. Reduce the exhaust ventilation rate

2. Optimize makeup air delivery to kitchen

3. Integrate the CKV system with the HVAC system

CKV/HVAC Optimization Strategies

1. Minimize design exhaust rate

- Group appliances according to effluent production and associated ventilation requirements.
- Engineered UL listed canopy hoods to increase effectiveness and reduce heat gain. Use proximity hoods where applicable.
- Side panels and end walls!

Download at: www.fishnick.com



Hood Setup over Two Charbroilers



8-Foot Wall Mounted Canopy Hood

Single-Island Canopy with Displacement MUA (C&C 5100 cfm, 2 charbroilers cooking)



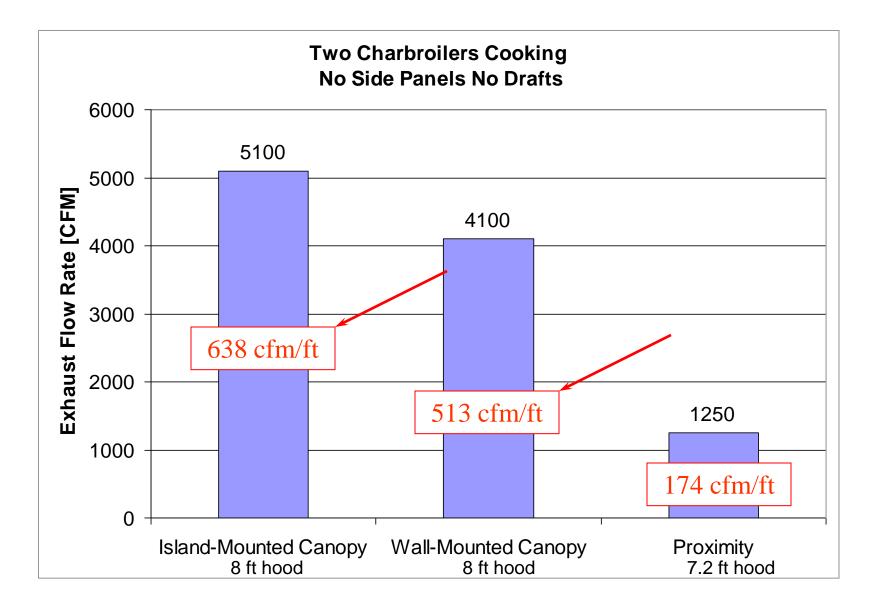
Wall Canopy with Displacement MUA (C&C 4100 cfm, 2 charbroilers cooking)



Proximity Hood with Displacement MUA (C&C 1250 cfm, 2 charbroilers cooking)

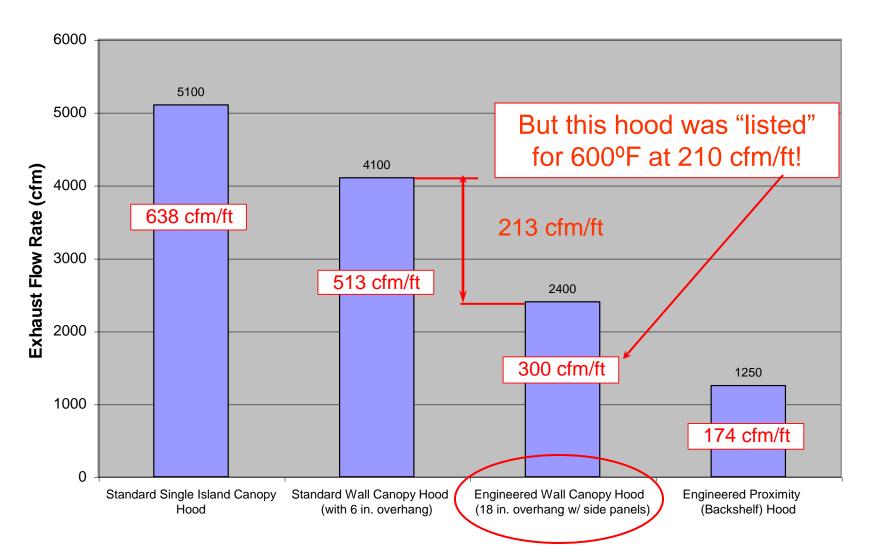


Hood Type Effect on C&C

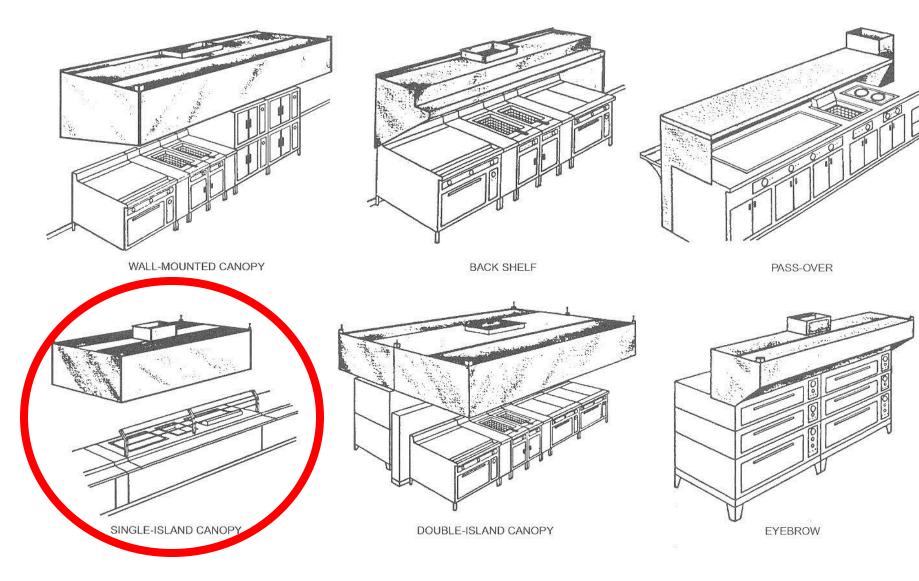


Add in an Engineered Wall-Canopy Hood

Two 3-Foot Charbroilers Cooking under an 8-Foot Hood



...let's look at the single-island hood in the lab



Single-Island Canopy Hood Charbroiler @ 600°F Idle Condition



Not that different from the real world!



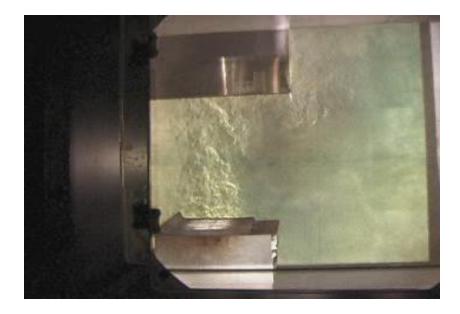


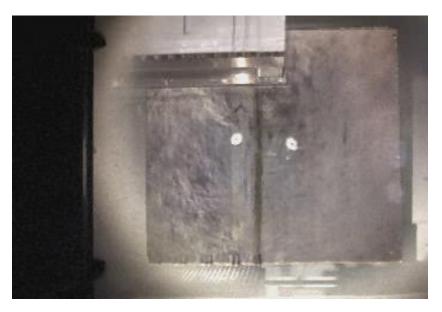


End View 12 inch front overhang

Front View 6 inch side overhang

Exhaust Rate: 300 cfm/ft



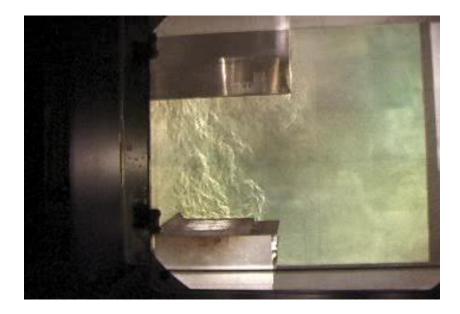


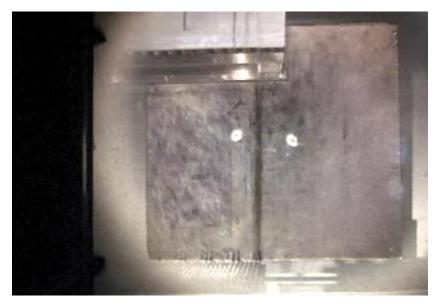
End View (Spill on Front Edge) Front View (Spill on Right Side)

4-Way Diffuser Set-up



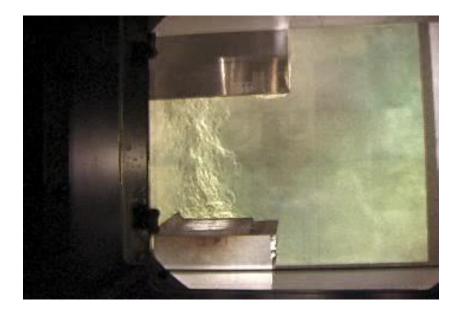
Exhaust Rate: 300 cfm/ft (with right 4-way turned on)

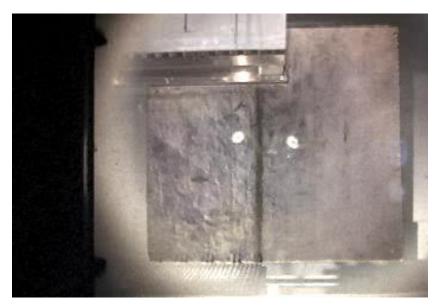




End View (Spill on Front Edge) Front View (Spill on Right Side)

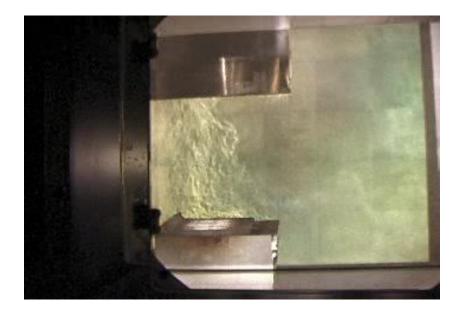
Exhaust Rate: 500 cfm/ft

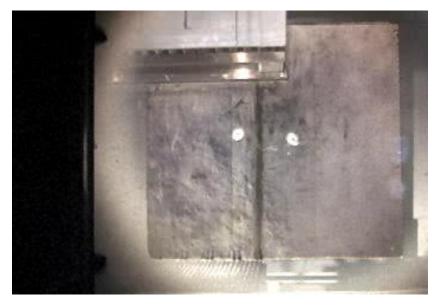




End View (No Spill on Front Edge) Front View (No Spill on Right Side)

Exhaust Rate: 500 cfm/ft (with right 4-way turned on)

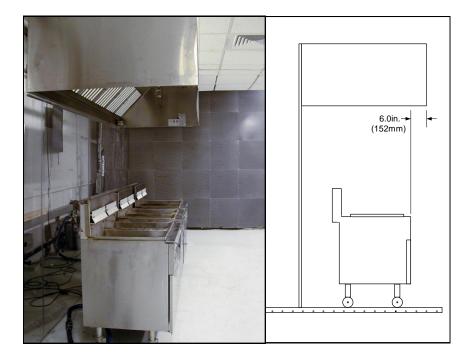




End View (No Spill on Front Edge) Front View (Spill on Right Side) Bottom Line: Single-Island Canopy Hoods and Charbroilers Don't Mix Well!

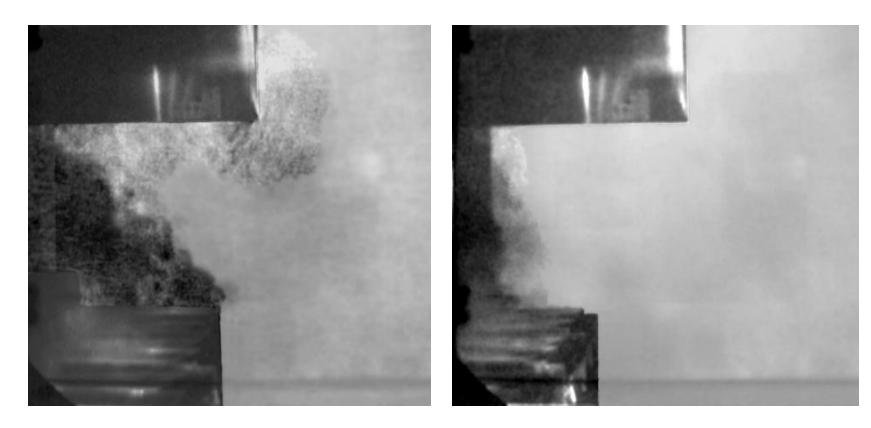
...let's go back into the lab

Overhang Impacts Hood Performance!





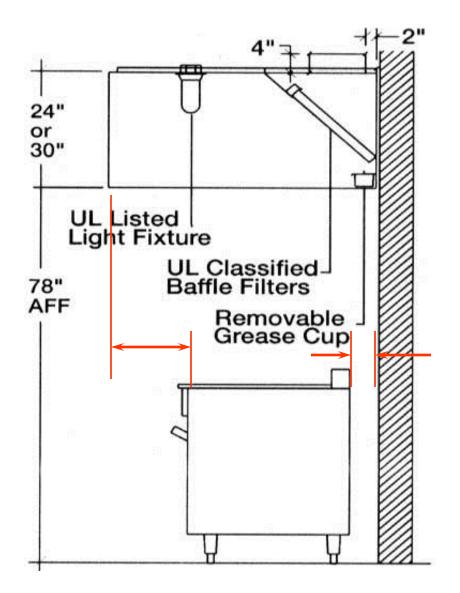
Overhang effect for 6 fryers under a 10-ft. wall canopy hood at 2400 cfm (240 cfm/ft)



6 inches of Front Overhang

18 inches of Front Overhang

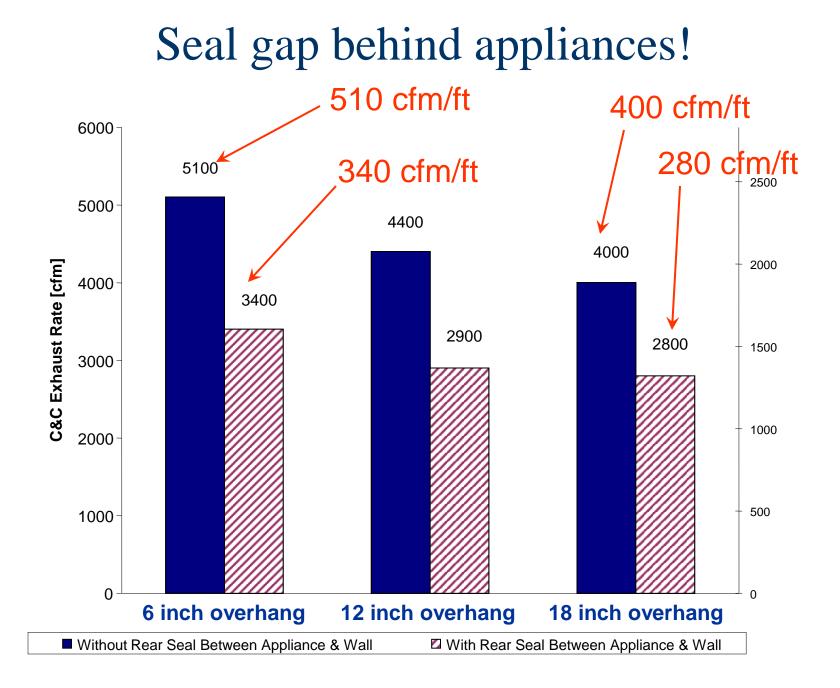
Overhang vs. Rear Gap



Rear Seal Investigation



Front Overhang to Appliance [inches]	Front Overhang to Cooking Surface [inches]	Distance Between the Rear of the Appliance and Backwall [inches]
0	6.0	→ 16.5
6.0	12.0	→ 10.5
12.0	18.0	→ 4.5



Dynamic Effect - Oven Door (6")



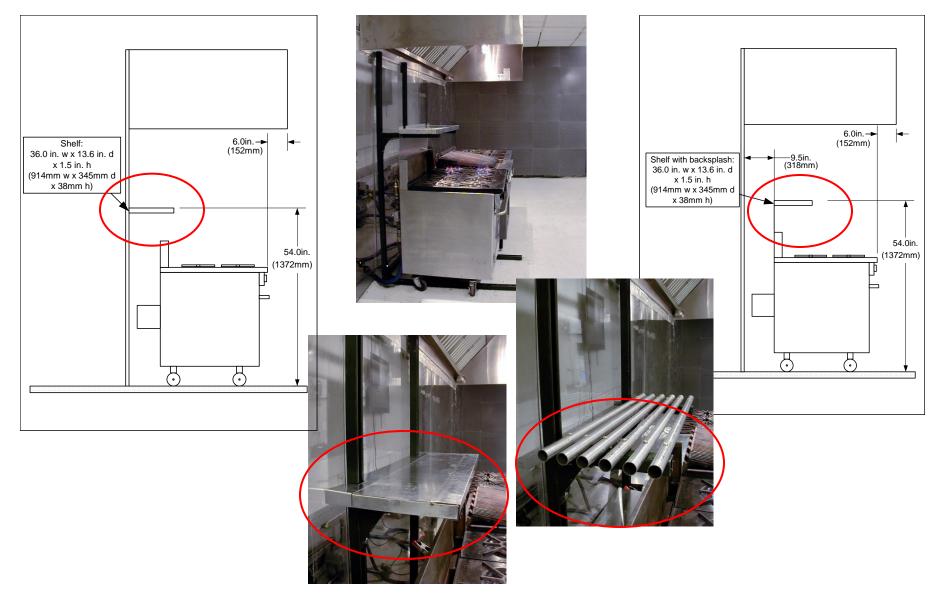
Dynamic Effect - Oven Door (18")



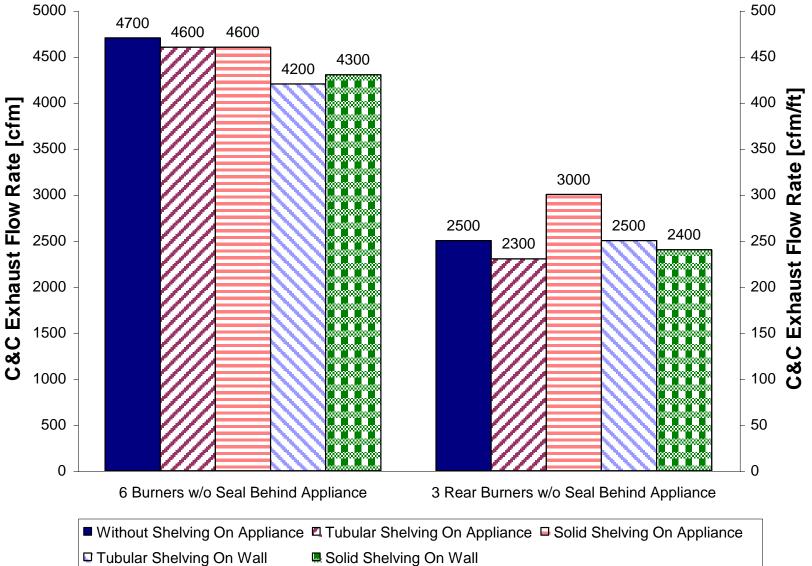
...easier "said" than "done"



Shelving over a 6-burner Range

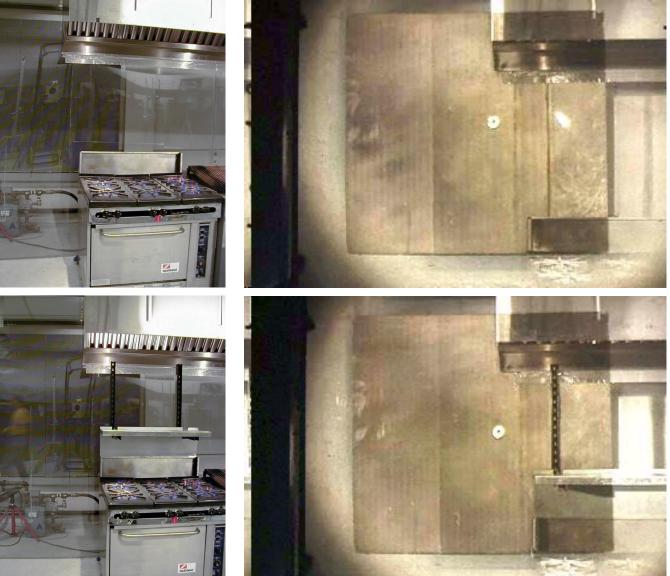


Shelving over a 6-Burner Range Results



6-burner Range C&C Comparison Without Shelf & With Solid Shelf

4700 cfm (470 cfm/ft)

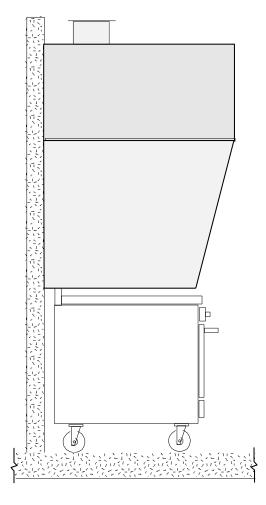


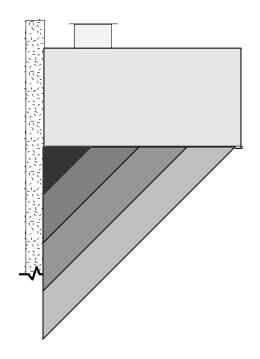
4600 cfm (460 cfm/ft)

Side Panel Benefit

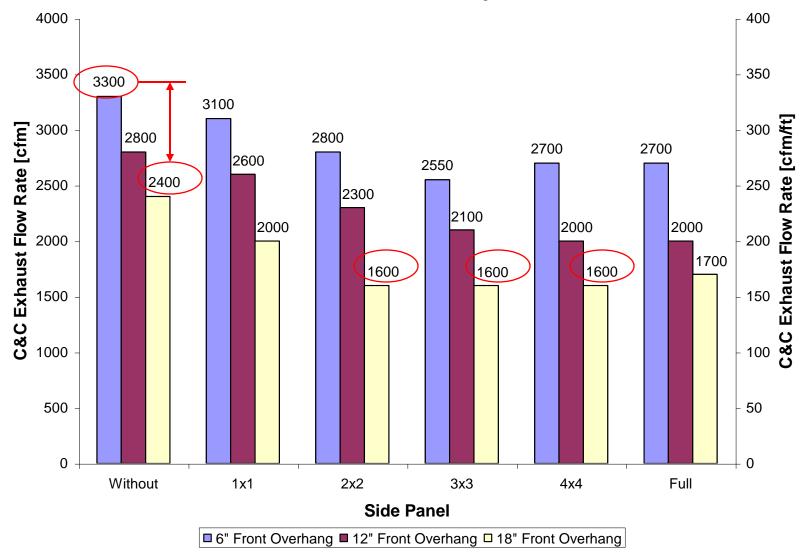
Effect on C&C from:

- •Full-side panels
- •4ft x 4ft tapered
- •3ft x 3ft tapered
- •2ft x 2ft tapered
- •1ft x 1 ft tapered

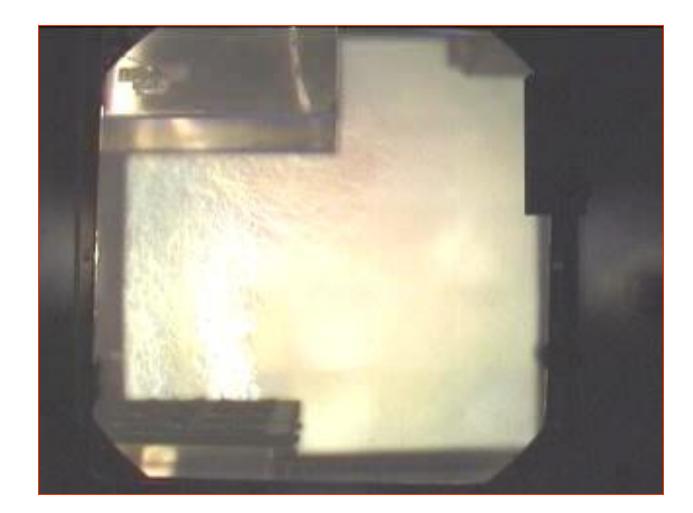




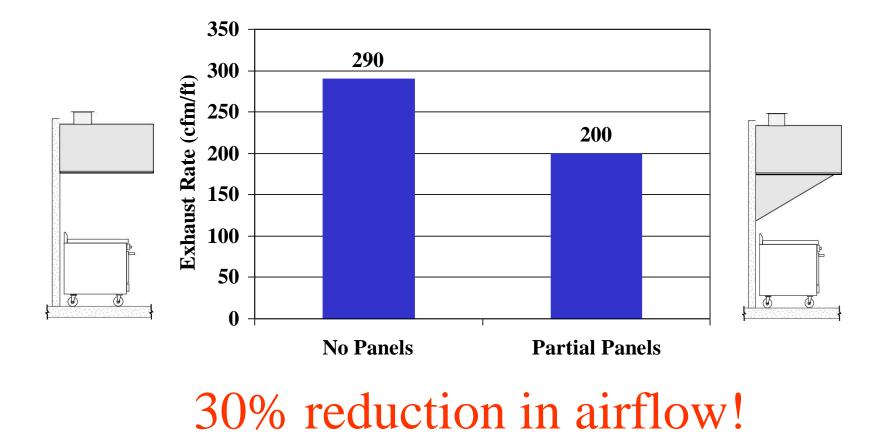
Side Panels/Overhang Results for Fryers



... partial end panels do the job!



Multiple configurations of appliances under various 10-ft. wall canopy hoods (approx. 90 tests) with and without partial side panels



The Effect of Hood Depth

4 ft Depth Increased to 5 ft

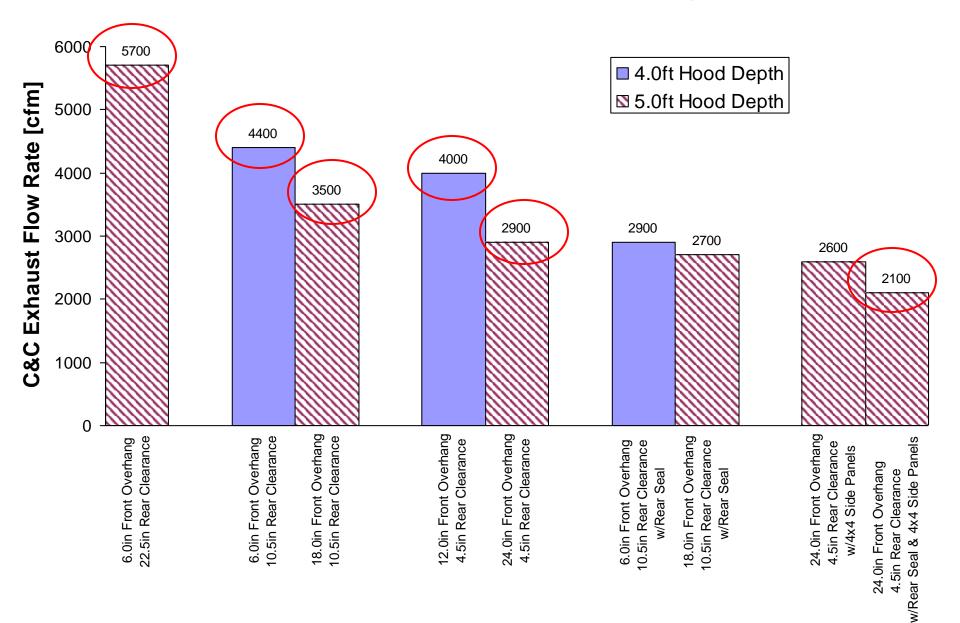




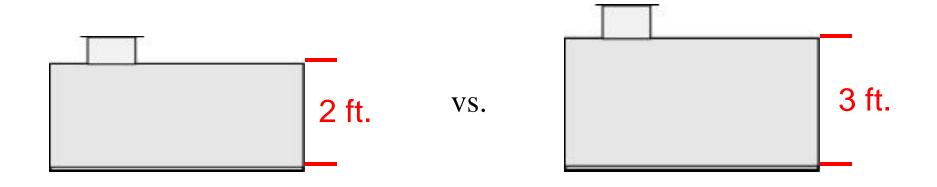
6 inch overhang

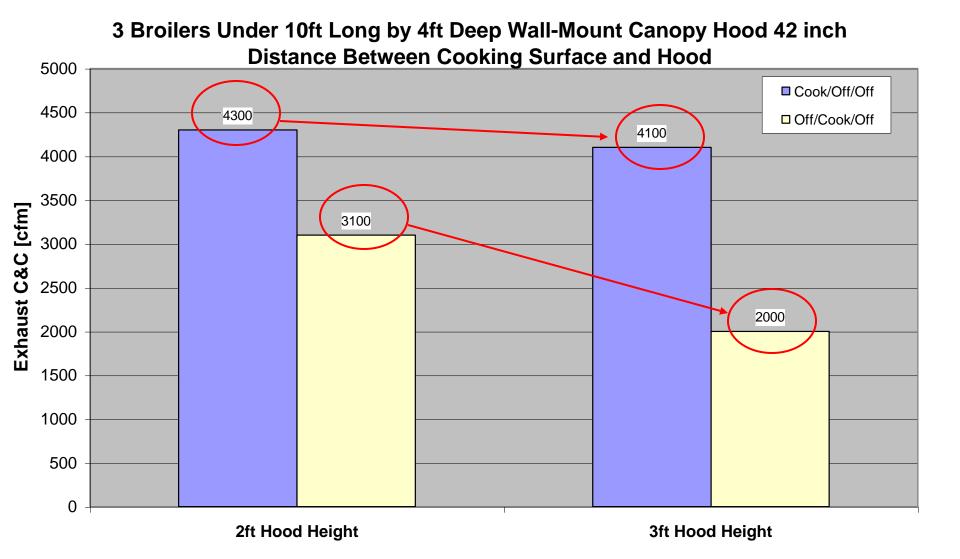
24 inch overhang

3 Charbroilers Cooking

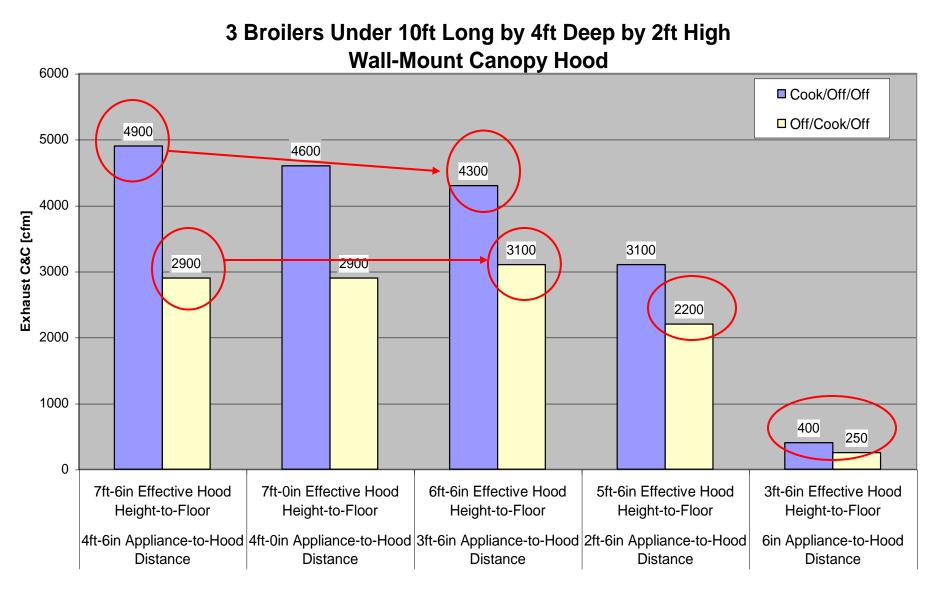


The Effect of Hood Height Itself





The Effect of Hood Mounting Height



Total exhaust approx... 600 cfm



Hoods are not created equal...



Tools for the Tool Box:

- Bigger hoods
 - Deeper
 - Taller
- Push back equipment (minimize rear gap)
- Lower hoods (or proximity style where practical)
- Side panels, end panels, end walls!
- Heavy duty (broiler) in middle
- Light duty (ovens) on the end
- Don't waste hood space over non-cooking
- Introduce makeup air at low velocity.

CKV/HVAC Design Strategies

2. Optimize makeup air delivery to kitchen

- No short-circuit hoods!
- Introduce replacement air at low-velocity

Design Guide 2 Commercial Kitchen Ventilation Optimizing Makeup Air

This design guide provides information that will help achieve optimum performance and energy efficiency in commercial kitchen ventilation systems. The information presented is applicable to new construction and, in many instances, retrofit construction. The audience for this guideline is kitchen designers, mechanical engineers, food service operators, property managers, and maintenance people. This guide is intended to augment comprehensive design information published in the Kitchen Ventilation Chapter in the ASHRAE Handbook on HVAC Applications as well as Design Guide No. 1: Commercial Kitchen Ventilation - Exhaust Hood Selection & Sizing.

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Influence of Makeup Air	5
MUA Recommendations	6
Influence of Other Factors	9
Energy Saving Considerations	6
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Introduction

An effective commercial kitchen ventilation (CKV) system requires balance—air balance that is. And as the designer, installer or operator of the kitchen ventilation system, you may be the first person called upon to perform your own "balancing act" when the exhaust hood doesn't work. Unlike a cooking appliance, which can be isolated for troubleshooting, the exhaust hood is only one component of the kitchen ventilation system. To further complicate things, the CKV system is a subsystem of the overall building heating, ventilating and air-conditioning (HVAC) system. Fortunately, there is no "magie" to the relationship between an exhaust hood and its requirement for replacement or makeup air (MUA). The physics are simple: air that exits the building (through exhaust hoods and fans) must be replaced with outside air that enters the building (intentionally or otherwise). The essence of *air bulance*. "air in" a "air out"

Background

If the replacement air doesn't come in, that means it doesn't go out the exhaust hood and problems begin. Not only will the building pressure become too "negative," the hood may not capture and contain (C&C) cooking effluents due to reduced exhaust flow. We have all experienced the "can't-open-the-door" syndrome because the exhaust fan is sucking too hard on the inside of the restaurant. The mechanical design may call for 8000 cubic feet per minute (cfm) of air to be exhausted through the hood. But if only 6000 cfm of outdoor air is able to squeeze in through closed dampers on rooftop units and undesiable pathways in the building envelope, then only 6000 cfm is available to be exhausted through the hood. The exhaust fan creates more suction (negative pressure) in an unsuccessful attempt to pull more air through the hood.

There is no piece of equipment that generates more controversy within the food service equipment supply and design community than the exhaust hood in all its styles and makeup air combinations. The idea that by not installing a dedicated

CKV/HVAC Optimization Strategies

- 3. Integrate the CKV system with the HVAC system
 - Maximize dining room outdoor air as replacement air for the hood/minimize local makeup air.
 - Consider using HVAC system to replace 100% makeup air.
 - Consider demand ventilation controls (DVC) to kitchen exhaust integrate with MUA and/or HVAC outdoor air supply

Design Guide 3

Improving Commercial Kitchen Ventilation System Performance Integrating Kitchen Exhaust Systems with Building HVAC

This design guide provides information that may help achieve optimum performance and energy efficiency in communical kitchen werkens by information systems by information and an energy and and and information and an energy and and information and an energy and and some instances, nettoric construction. The audience for this guideline is kitchthe audience for this guideline is kitchnoored instances, nettoric construction. The audience for this guideline is kitchpoperty managers, and maintanace people. The building code analysis is to approximation of the audience of the ASIRAE handbook on HVAC Applace Market is instanded to augerest or prohensive design information published in the Kitchen Vertification Chapter in the ASIRAE handbook on HVAC Applace under the design corners sublished for proving Commercial Kitchen Vertification System Performance.



The Opportunity: Reduce Utility Costs and Improve Kitchen Comfort

The replacement air required for commercial kitchen ventilation systems is always 100% of the exhaut aim—what goes out must come in A common design practice is to rupply at least 50% of replacement air using an independent makeny air wait (JACU) with the remaining 20% supplied by conditioned outside air from heating, ventilating, and air-conditioning (HVAC) root-top units (RTU) serving the kitchen and/or by transfer air from adjacent spaces. This keeps the kitchen under a negative pressue (eiktive to the dining room) to percent cooking odors from migrating into the dining sea. In many climates the explorement air from an independent makeny air unit is not conditioned, which may cease unconfortable conditions (too cold and/or too to) in the kitchen. In other climates, the makeny air is hested, which in many cases result in inumlicances heating (by the MAU) and cooling (by the RTU) of the kitchen during the shoulder season. Coarventional design practice does not take full advantage of the relatively high rate of occupancy ventilation situ is instoded into the dining coon or other sease of the building adjacent to the kitchen.

These is an opportunity to use code-sequized outdoor air supply to the dising room as sepacement air, thus reducing or eliminating the fraction of replacement air from the independent makeup air unit. Since occupancy ventilation air is conditioned in most cases, transferming it to the kitchen as a contribution to the replacement air sequirement can improve comfort conditions in the kitchen.

The other design guides in this series explain the principles for selecting and using exhaust boods, as well as the fundamental of introducing replacement air to avoid degrading exhaust bood capture and containment. This guide explains the advantages and challenges of integrating replacement air with the building HVAC system to maximize the use of occupancy ventilation air as replacement air. The *l'omitains* section describes how outside air requirements are calculated based on occupancy or conditioned floor area. The Food Service HVAC section discusse design issues related to relection and occutol of control HVAC

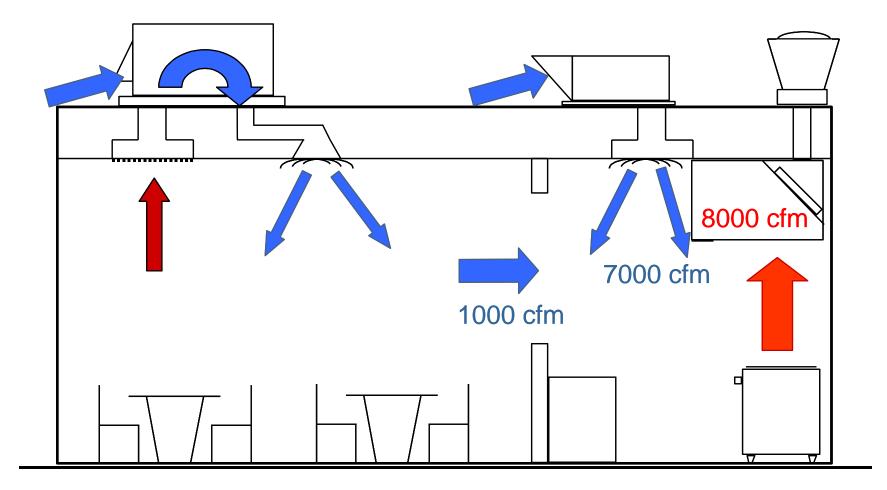
Free Download:

http://www.fishnick.com/equipment/ckv/designguides/

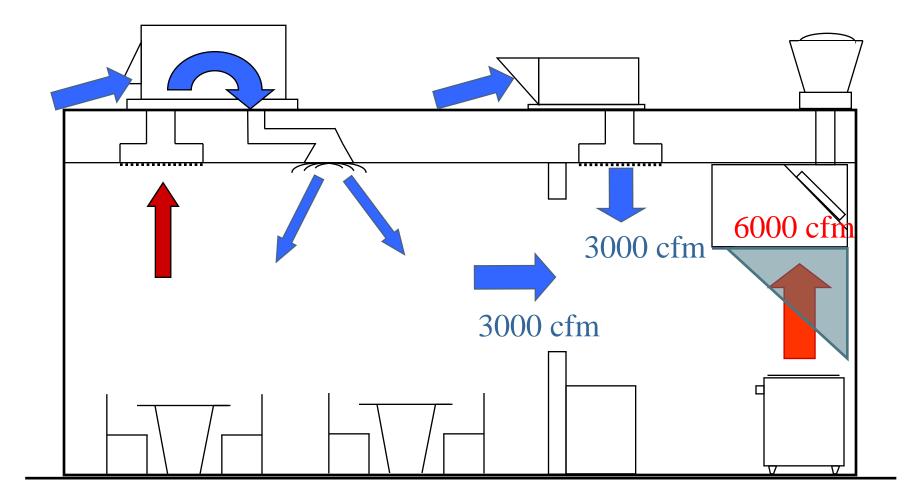
What does CKV-HVAC integration really mean?

Conversely, what does NOT integrating CKV with HVAC mean?

Non-Integrated Approach



Integrated HVAC with CKV!



The first question to be answered is: *How much occupancy ventilation air is available for use as transfer air*?

1) 0.20 cfm x ft2

or

2) 15 cfm/person x maximum occupancy

Select the greatest of the two. In restaurants, 2) will always be the larger value.

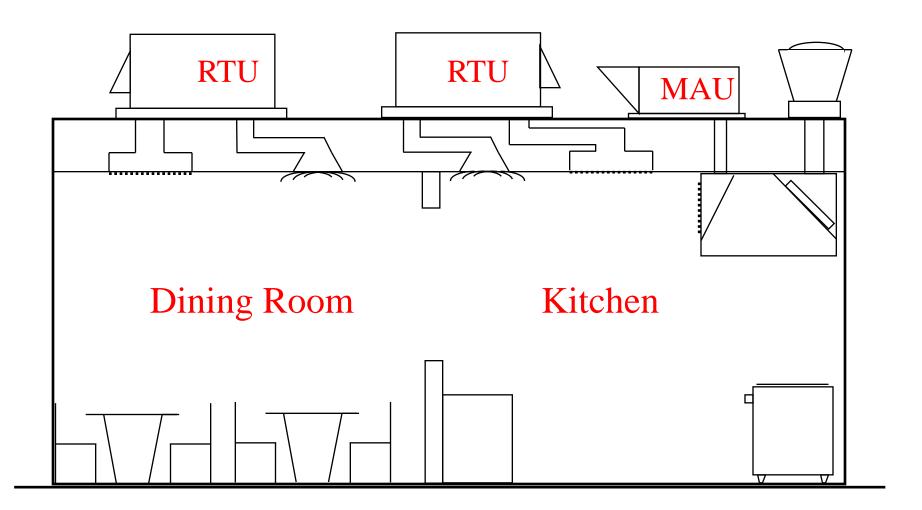
The second question to be answered is: *How will selecting and sizing of heating, ventilating, and air-conditioning (HVAC) equipment affect the availability of replacement air?*

The answer varies significantly. A design could specify multiple 5 ton RTUs (to avoid economizers), larger RTUs to minimize cost, or a single 100% dedicated replacement air unit (RAU) to supply all ventilation air needs of the facility. The design guide discusses this in depth.

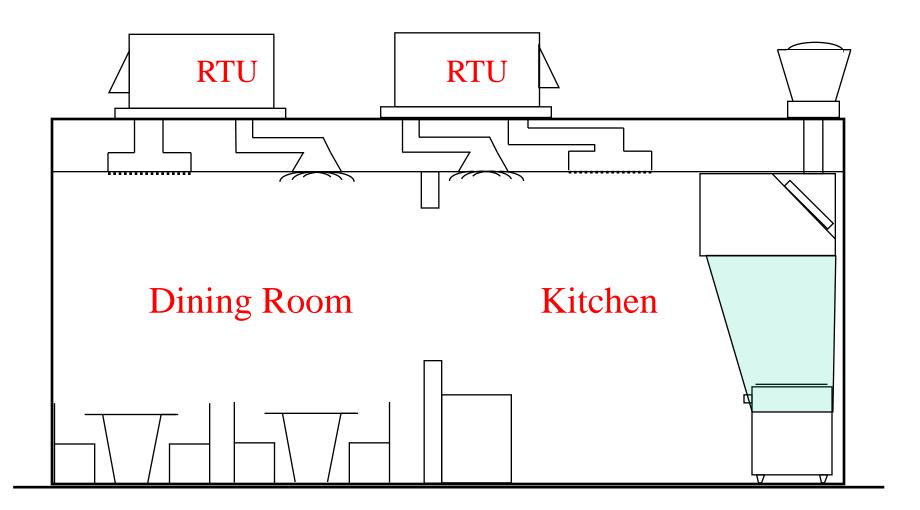


Ventilates, Cools, Dehumidifies & Heats Using 100% Outdoor Air

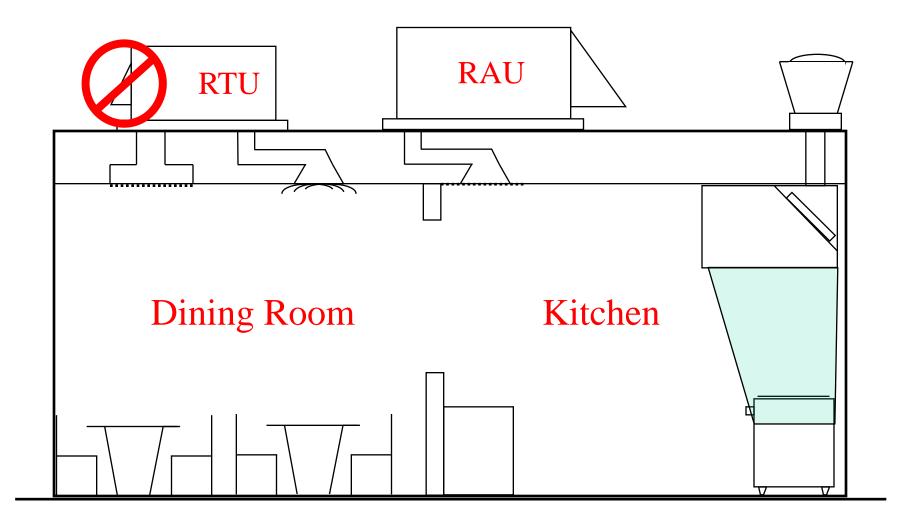
Replacement Air Strategy #1



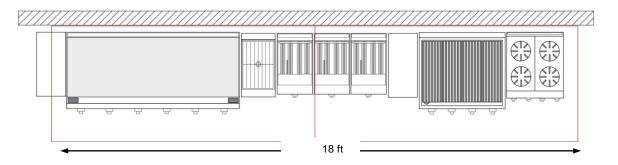
Replacement Air Strategy #2



Replacement Air Strategy #3



Base Case Cookline & Exhaust Hood





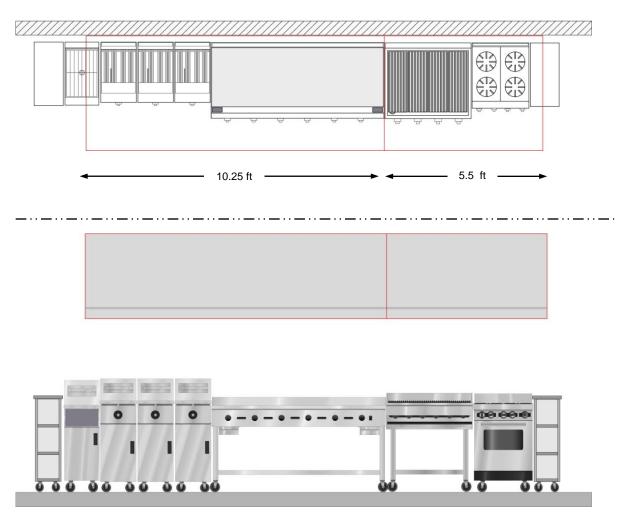


Design Exhaust = 7200 cfm (400 cfm/ft x 18 ft)

Table B-1. Casual Dining Base Case Air Balance.

Replacement and Exhaust Air	Maximum Outside Air for Occupancy (cfm)	Minimum Outside Air for Occupancy (cfm) 10% of Max	Outdoor (Replacement) Air Available for Kitchen Exhaust (cfm)	Exhaust Air (<u>cfm</u>)	Supply Air (cfm)	Nominal Cooling Capacity (refr. Tons)	Outside Air Fraction [OA/SA] %	SA <u>cfm</u> /ton
Dining Room Rooftop Unit #1 (RTU-1)	1050	125	400		4800	12	22%	400
Dining Room Rooftop Unit #2 (RTU-2)	675	80	200		3000	7.5	23%	400
Dining Room Rooftop Unit #3 (RTU-3)	675	80	200		3000	7.5	23%	400
Kitchen Rooftop Unit (RTU-4)	300	300	1200		4800	12	25%	400
Makeup Air Unit (sized at 80% of hood exhaust)			5800				100%	
Restroom Exhaust				300				
Dry Storage Exhaust				100				
Kitchen Hood Exhaust				7200			_	
Total	2700	585	7800	7600	15600	39	23%	
Net Outdoor Air for Building Pressurization			200					

Case I: Cookline & Exhaust Hoods



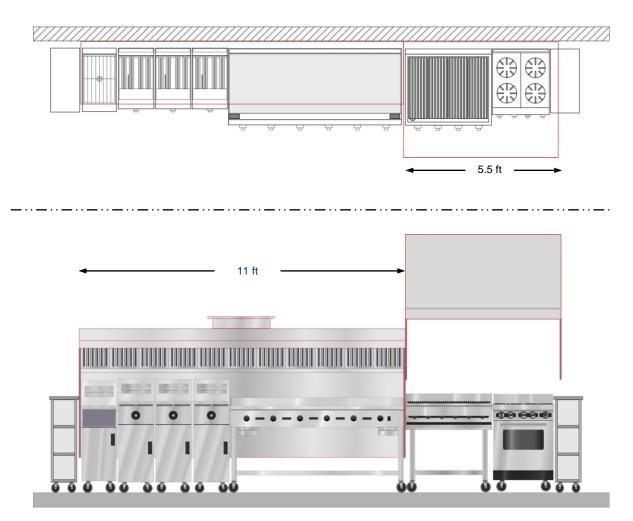
Hood over griddle & fryers: 10.25 ft. x 250 cfm/ft = 2,560 cfm Hood over broiler & range: 5.5 ft. x 400 cfm/ft = 2,200 cfm Total Exhaust Rate: 4760 cfm Design @ 4800 cfm

Table B-2. Case I Optimized Design Air Balance withEngineered Hoods and MAU Size Reduced.

Replacement and Exhaust Air	Maximum Outside Air for Occupancy (cfm)	Minimum Outside Air for Occupancy (cfm) 10% of Max	Outdoor (Replacement) Air Available for Kitchen Exhaust (cfm)	Exhaust Air (<u>cfm</u>)	Supply Air (cfm)	Nominal Cooling Capacity (<u>refr</u> . Tons)	Outside Air Fraction [OA/SA] %	SA <u>cfm</u> /ton
Dining Room Rooftop Unit #1 (RTU-1)	1050	110	900		4800	12	19%	400
Dining Room Rooftop Unit #2 (RTU-2)	675	70	600		3000	7.5	20%	
Dining Room Rooftop Unit #3 (RTU-3)	675	70	600		3000	7.5	20%	
Kitchen Rooftop Unit (RTU-4)	300	300	600		4800	12	13%	400
Makeup Air Unit (sized at 33% of hood exhaust)			2600					
Restroom Exhaust				300				
Dry Storage Exhaust				100				
Kitchen Hood Exhaust				4800			_	
Total	2700	550	5300	5200	15600	39	17%	
Net Outdoor Air for Building Pressurization			100					

Without consideration for HVAC outdoor air, the MUA unit could have been sized at 80 to 90% or approx. 4000 cfm

Case II: Cookline & Exhaust Hoods



Custom backshelf hood over griddle & fryers: 11 ft. x 150 cfm/ft = 1,650 cfm Custom canopy hood with full side panels over broiler & range: 5.5 ft. x 300 cfm/ft = 1,650 cfm Total Exhaust Rate: 3,300 cfm

Table B-3. Case II Optimized Design Air Balance withMaximum Transfer Air and Eliminated MAU.

Replacement and Exhaust Air	Maximum Outside Air for Occupancy (cfm)	Occupancy	Outdoor (Replacement) Air Available for Kitchen Exhaust (cfm)	Exhaust Air (cfm)	Supply Air (cfm)	Nominal Cooling Capacity (refr. Tons)	Outside Air Fraction [OA/SA] %	SA cfm/ton
Dining Room Rooftop Unit #1 (RTU-1)	1050	n/a	1200		4800	12	25%	400
Dining Room Rooftop Unit #2 (RTU-2)	675	n/a	700		3000	7.5	23%	
Dining Room Rooftop Unit #3 (RTU-3)	675	n/a	700		3000	7.5	23%	
Kitchen Rooftop Unit (RTU-7)	300	n/a	1200		4800	12	25%	400
Restroom Exhaust				300				
Dry Storage Exhaust Kitchen Hood Exhaust				100 3300				
Total	2700		3800	3700	15600	39	24%	
Net Outdoor Air for Building Pressurization			100					

Note: MUA unit has been eliminated!!!

CKV-HVAC Integration Recap:

- 1. Optimize hood design and reduce the design exhaust airflow rate.
- 2. Optimize makeup air delivery to kitchen minimize impact on hood performance.
- 3. Maximize transfer air/minimize local makeup air.
- 4. Strive for 100% replacement air through HVAC units (versus using a conventional MAU unit without cooling), or...
- Consider using a dedicated 100% replacement air unit (RAU).
- 6. Apply demand ventilation control of hoods where cost effective.

The Fan Factor!

C.,

EFI

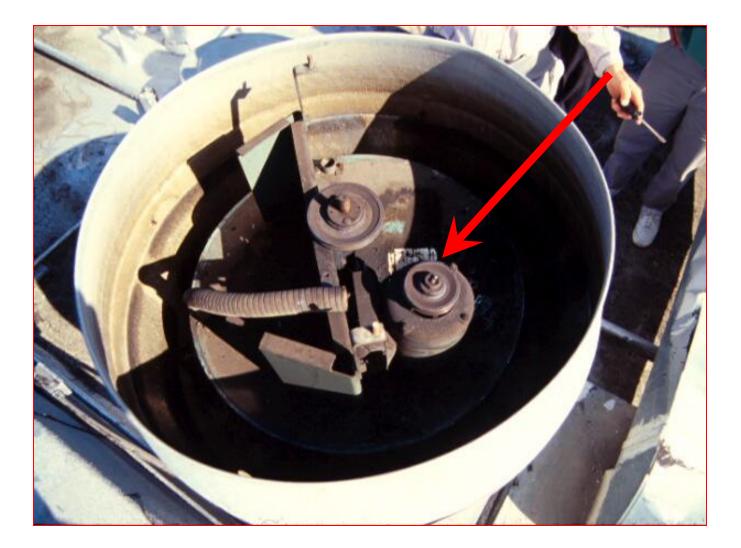
Hood static pressures* vary significantly (affecting fan energy directly)

Table 4 Exhaust Static Pressure Loss for Type I Hoods forVarious Exhaust Airflows

	Hood Static Pressure Loss, inches of water							
Type of Grease	150 to 250	250 to 350	350 to 450	500+				
Removal Device	cfm/ft	cfm/ft	cfm/ft	cfm/ft				
Baffle filter	0.25 to 0.50	0.50 to 0.75	0.75 to 1.00	1.00+				
Extractor	1.00 to 1.35	1.30 to 1.70	1.70+	1.70+				

*from the ASHRAE Handbook

Direct Drive Fans – the Future?



Variable Frequency Drives (VFD)



- Essentially electronic motor starters that replace magnetic starters
- Add flexibility to direct drive fans
- Separate Value Proposition from Demand Ventilation Controls (i.e., variable speed)

Now it time to consider....

Applying Demand Ventilation Control to Commercial Kitchen Ventilation?